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| 13. ABSTRACT (Maximum 200 words) <p>THIS INVESTIGATION WAS THE RESULT OF THE CONTINUED INTEREST IN INFILTRATION POTENTIAL IN CERTAIN PORTIONS OF THE RMA. PREVIOUS ESTIMATES OF INFILTRATION WERE BASED ON DATA PRESENTED IN SOIL SURVEY OF ADAMS COUNTY, CO (USDA SOIL CONSERVATION SERVICE AND COLORADO AG EXPERIMENT STATION, 1974). IN ORDER TO OBTAIN MORE SITE-SPECIFIC DATA, TEN SITES WERE SELECTED BY RMA PERSONNEL WHERE DOUBLE-RING INFILTRMETERS WOULD BE INSTALLED AND THEN LEFT IN PLACE. THESE SITES ARE IN THE SOUTH PLANTS AREA AND IN BASIN A.</p> <p style="text-align: right;">DTIC QUALITY INSPECTED 4</p> | | | |
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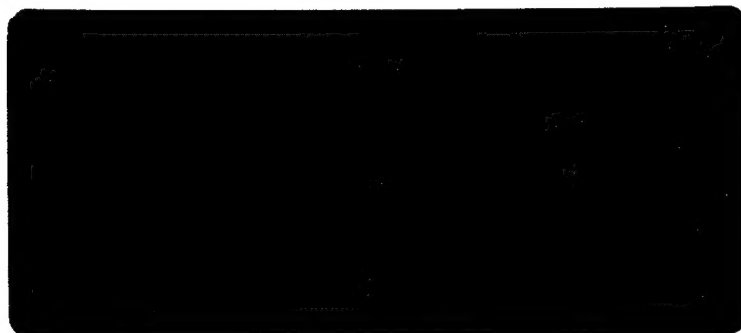


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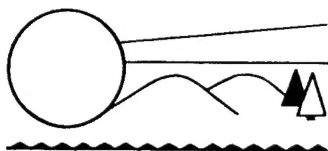
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RESULTS OF DOUBLE RING
INFILTRMETER INVESTIGATIONS
ROCKY MOUNTAIN ARSENAL
JULY 13-15, 1983



Introduction

This investigation was the result of the continued interest in infiltration potential in certain portions of the Rocky Mountain Arsenal. Previous estimates of infiltration were based on data presented in Soil Survey of Adams County, Colorado (USDA Soil Conservation Service & Colo. Ag. Exper. Station, 1974). In order to obtain more site-specific data, ten sites were selected by Rocky Mountain Arsenal personnel where double-ring infiltrometers would be installed and then left in place. These sites are in the South Plants Area and in Basin A. Fig. 1 shows the location of all ten sites.

Infiltration is defined as the movement of water into the soil matrix from the surface of the soil. It is normally expressed as a rate (f), e.g., centimeters per hour, etc. Various factors will influence the rate, such as the soil type, vegetal cover, rate of rainfall (or the rate at which water is available to enter the soil), chemical properties of the soil and the water, etc. It is also important to note that infiltration will vary with time. On a dry soil the initial infiltration rate may be several times the final or equilibrium rate.

The basic equation governing infiltration is that developed by Horton (1935) which resulted from his work during the early 1930's. This relationship is:

$$f = f_c + (f_o - f_c) e^{-kt}$$

where

f = infiltration rate (depth/time) at time t

k = a constant for the decrease in f

f_c = final or equilibrium value of f

f_o = initial infiltration rate



INFILTRATION TEST SITES

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A dual ring infiltrometer was used for these investigations at the Rocky Mountain Arsenal. The procedures for this method are set forth in ASTM Procedure Number D 3385-75 (American Society for Testing and Materials, 1978). The procedure is also discussed by Johnson (1963) in U. S. Geological Survey Water-Supply Paper No. 1544-F.

The dual rings of the infiltrometer were constructed of 10-gauge metal. The inner ring has an inside diameter of 12 inches and the outside ring has an inside diameter of 18 inches. Both rings are 12 inches deep. The inside ring was driven into the soil matrix a depth of 2 inches and the outside ring was driven to a depth of 5 inches. Inside the inner ring and between the two rings a small diameter metal rod, sharpened at the tip, was used as a reference point so the water would be kept at the desired level of 3 inches. Figures 2 through 5 show a typical installation.

Results Obtained

Fig. 1 shows the locations of the two sites selected. A detailed description of each site is included in Appendix A. Figures 6 through 15 show the graphical determination of the infiltration rates over time. It is important to note that the tests conducted were under a "dry soil" condition. Complete numerical data for these ten sites are shown in Appendix B and the f_c values are shown in Table 1.

Table 1
Values of " f_c " for Each of the Ten Sites

| Site | $f_c \frac{1}{\text{cm/hr}}$ |
|------|------------------------------|
| 1 | 0.03 |
| 2 | 0.04 |
| 3 | 0.03 |
| 4 | Data not meaningful |
| 5 | 0.23 |
| 6 | 2.55 |
| 7 | 0.74 |
| 8 | 1.03 |
| 9 | 1.93 |
| 10 | 5.21 |

^{1/} Values were determined graphically from
Figures 6 through 16.

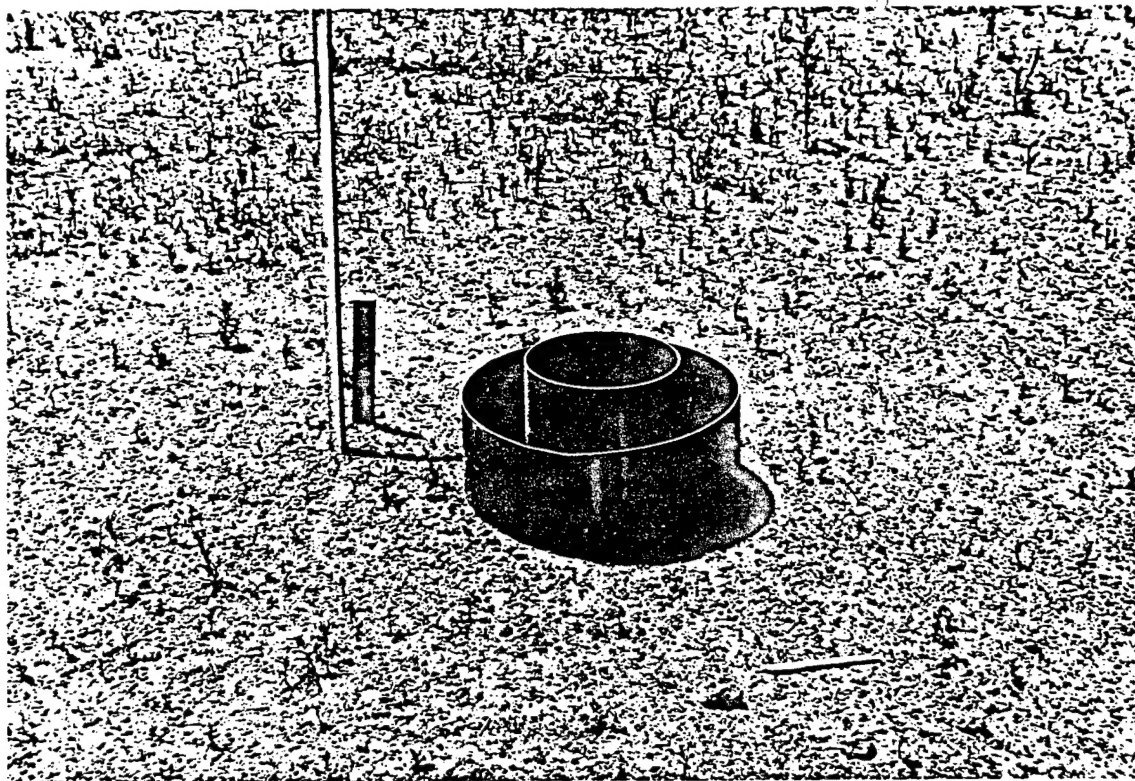


Fig. 2. Typical View of Double Ring Infiltrometer

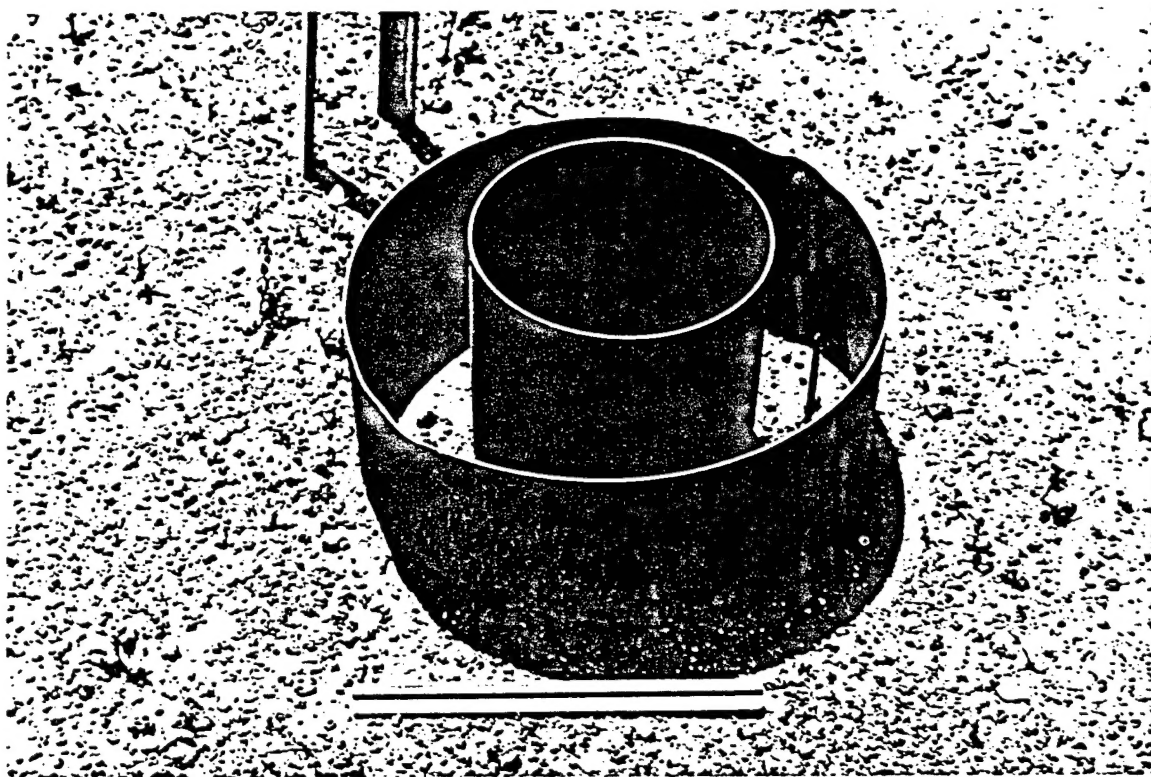


Fig. 3. Typical View of Double Ring Infiltrometer

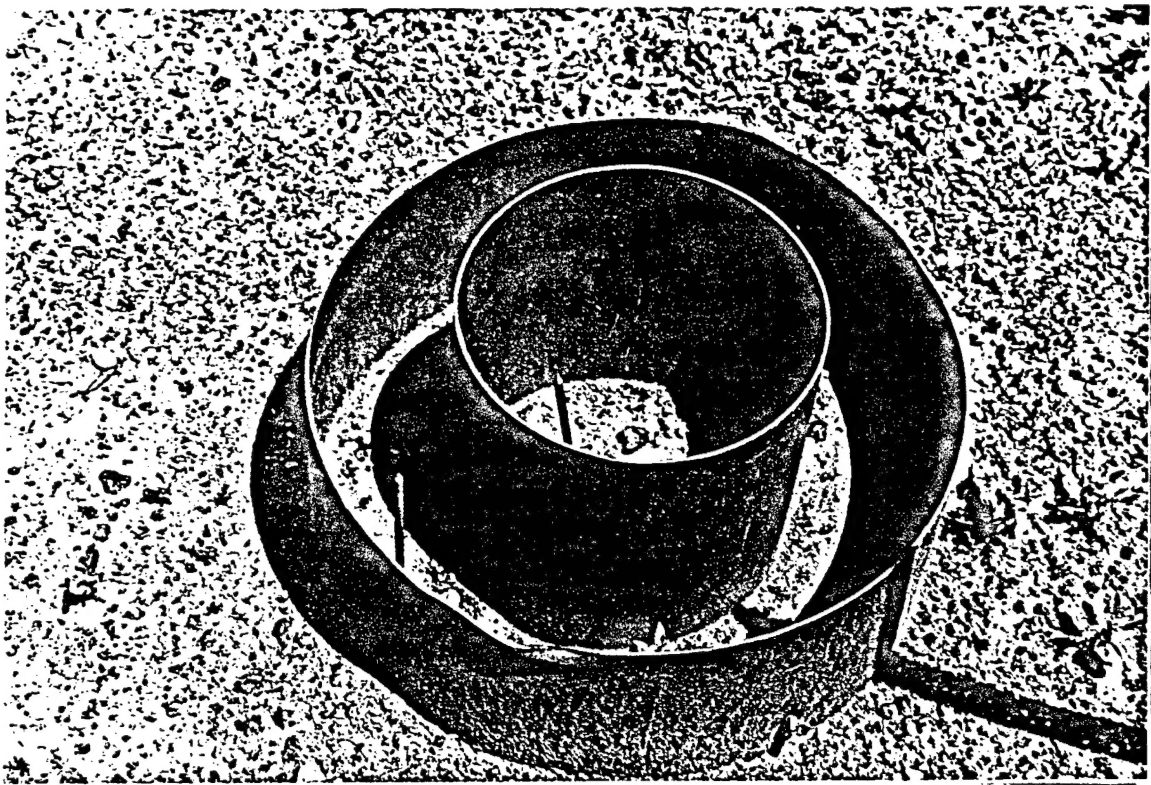


Fig. 4. Typical View of Double Ring Infiltrometer

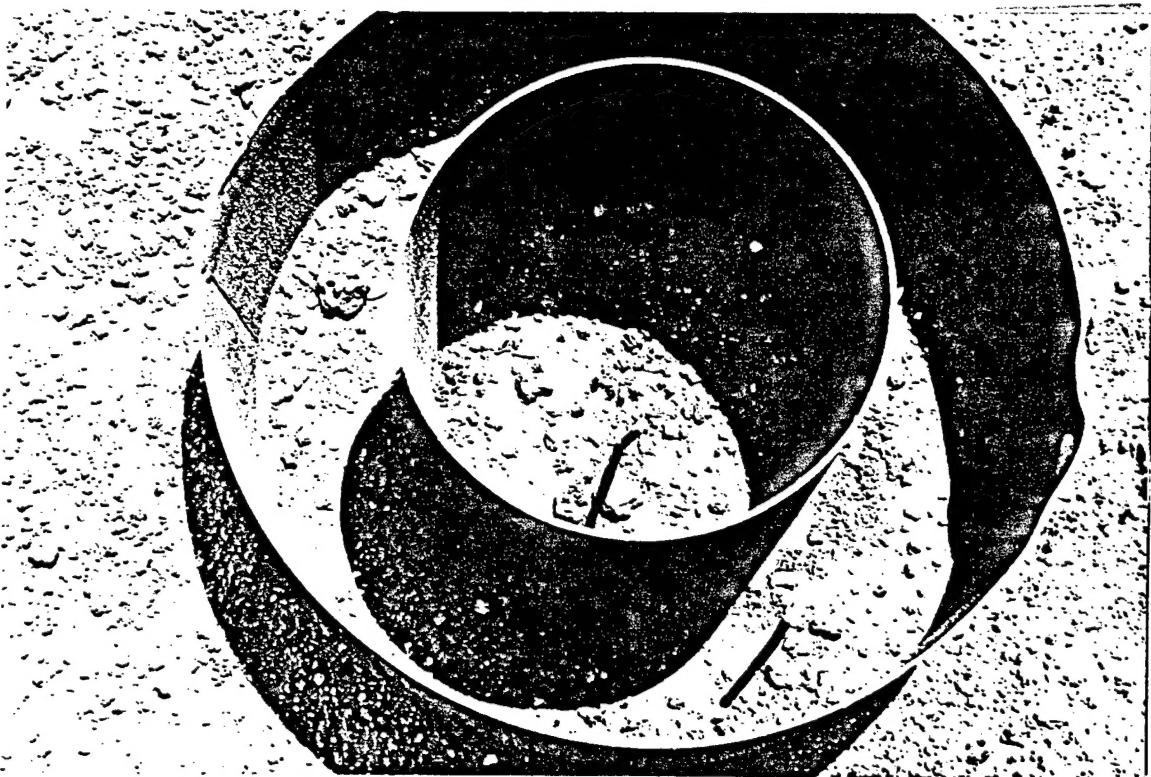


Fig. 5. Typical View of Double Ring Infiltrometer

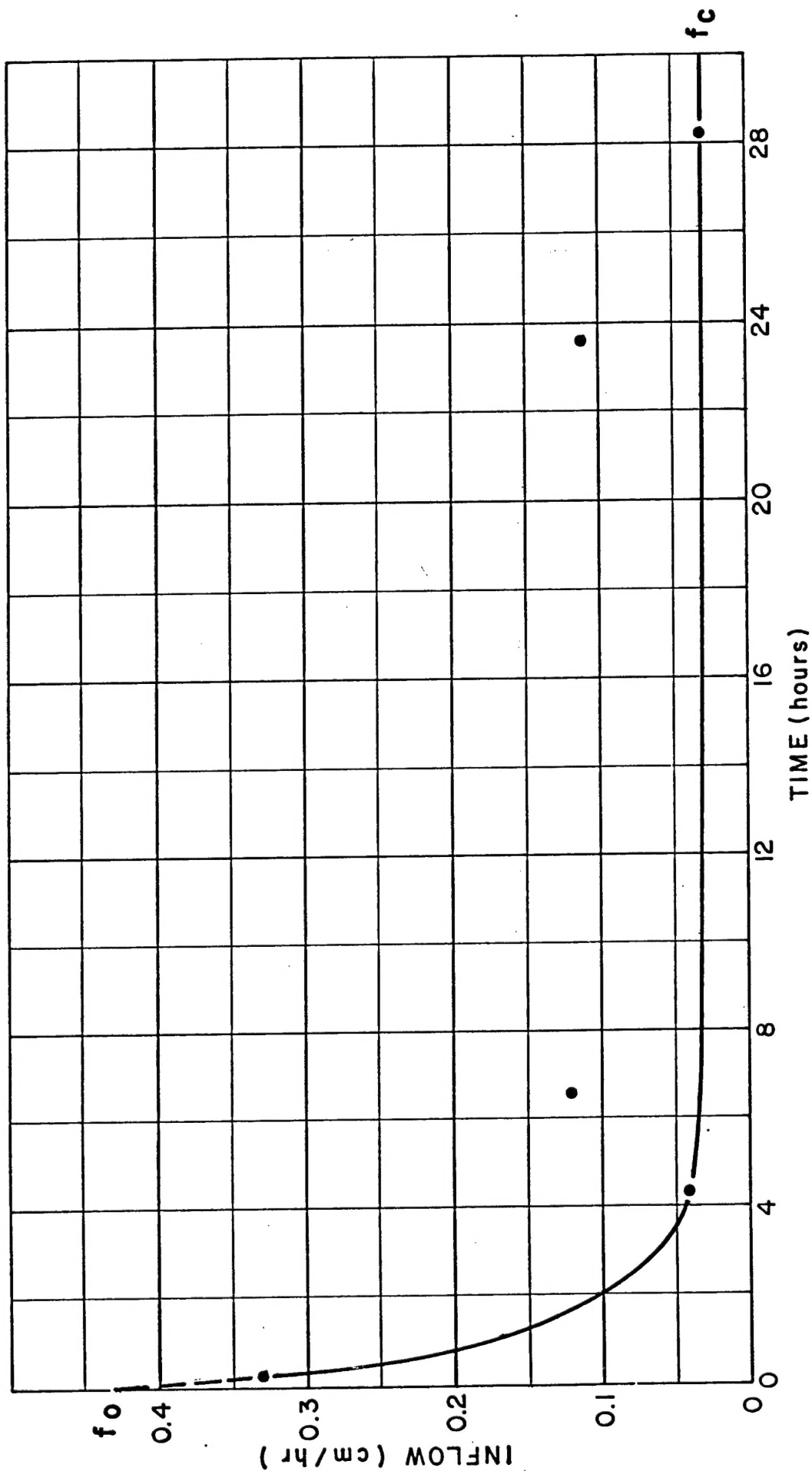


Fig. 6.

INFILTRATION SITE NO. 1

ROCKY MOUNTAIN ARSENAL
DENVER, COLORADO

RESOURCE CONSULTANTS, INC. - FORT COLLINS, COLORADO

7/14/83

7/15/83

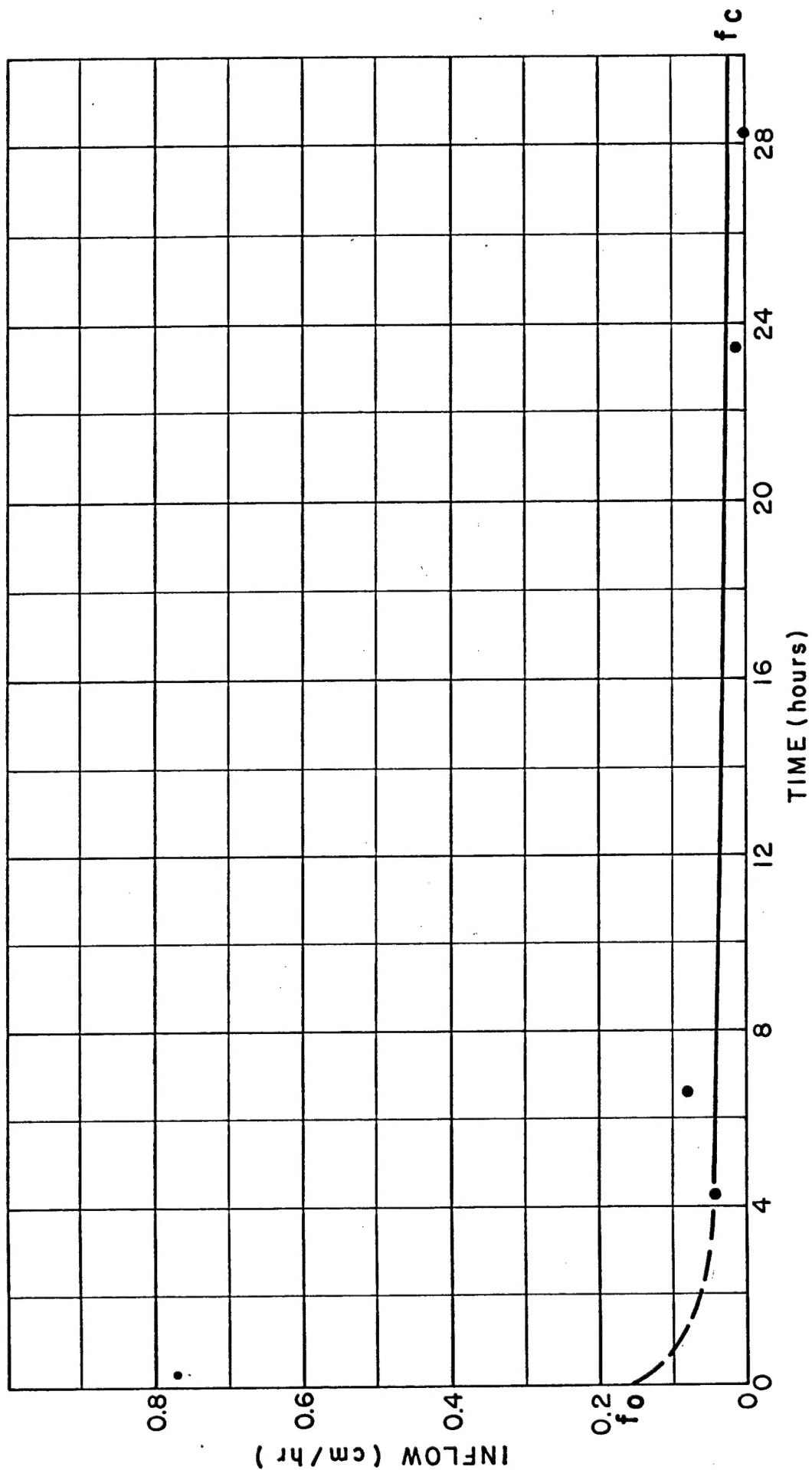


Fig. 7.

INFILTRATION SITE No. 2

ROCKY MOUNTAIN ARSENAL
DENVER, COLORADO

RESOURCE CONSULTANTS, INC. - FORT COLLINS, COLORADO

7/14/83

7/15/83

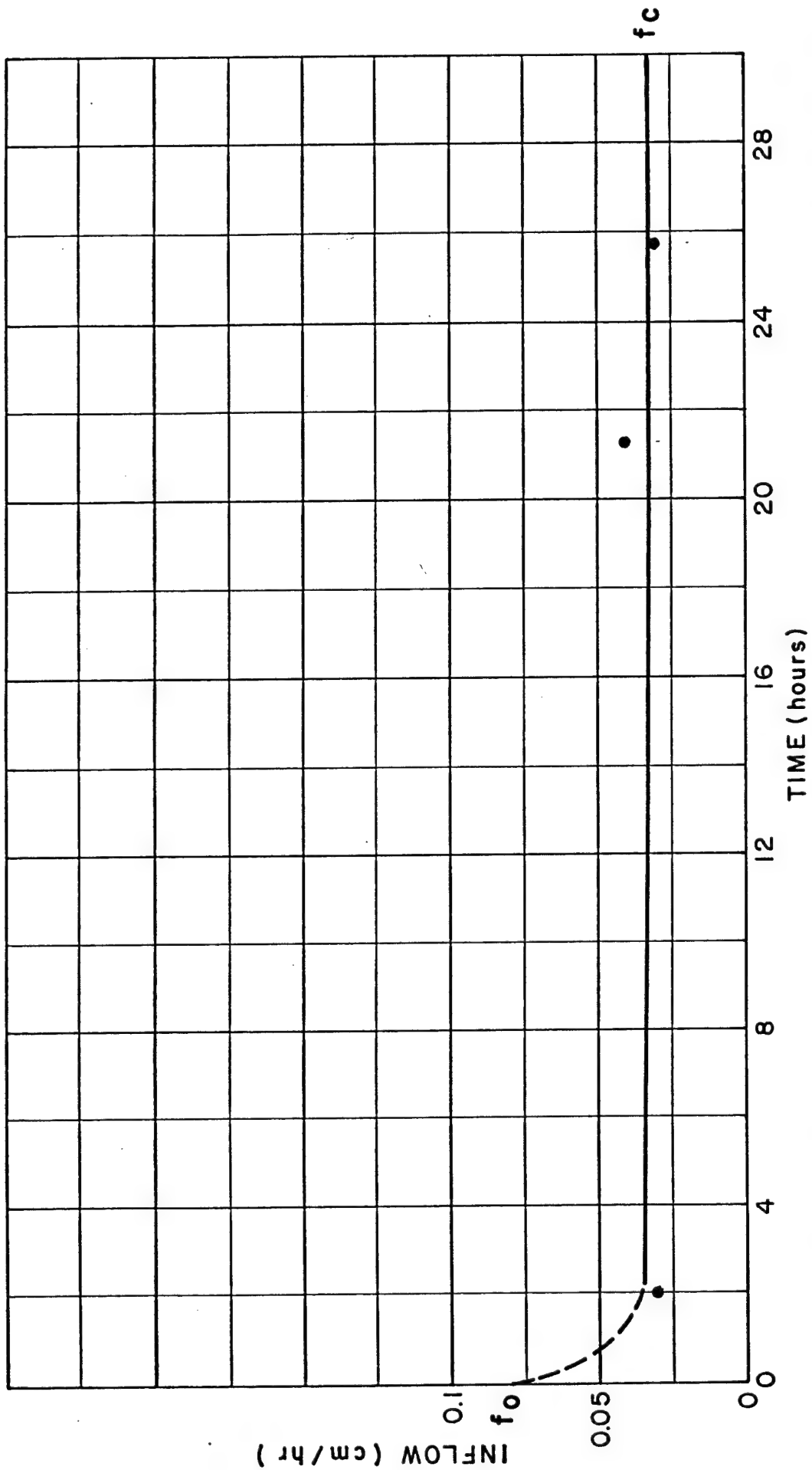


Fig. 8.

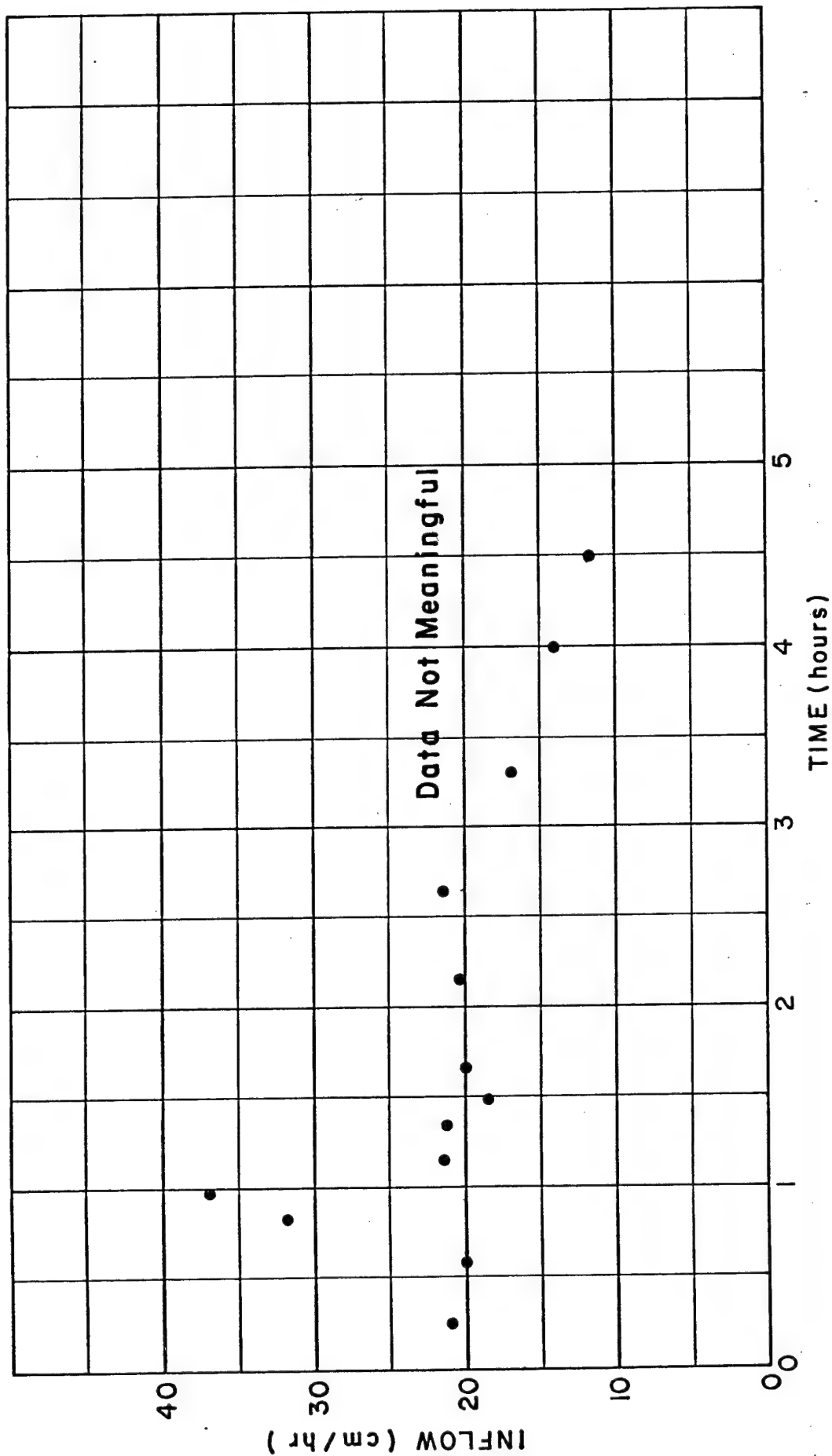
INFILTRATION SITE No. 3

ROCKY MOUNTAIN ARSENAL
DENVER, COLORADO

RESOURCE CONSULTANTS, INC. - FORT COLLINS, COLORADO

7/14/83

7/15/83



ROCKY MOUNTAIN ARSENAL
DENVER, COLORADO
RESOURCE CONSULTANTS, INC. - FORT COLLINS, COLORADO

Fig. 9.
INFILTRATION SITE No.4

7/14/83

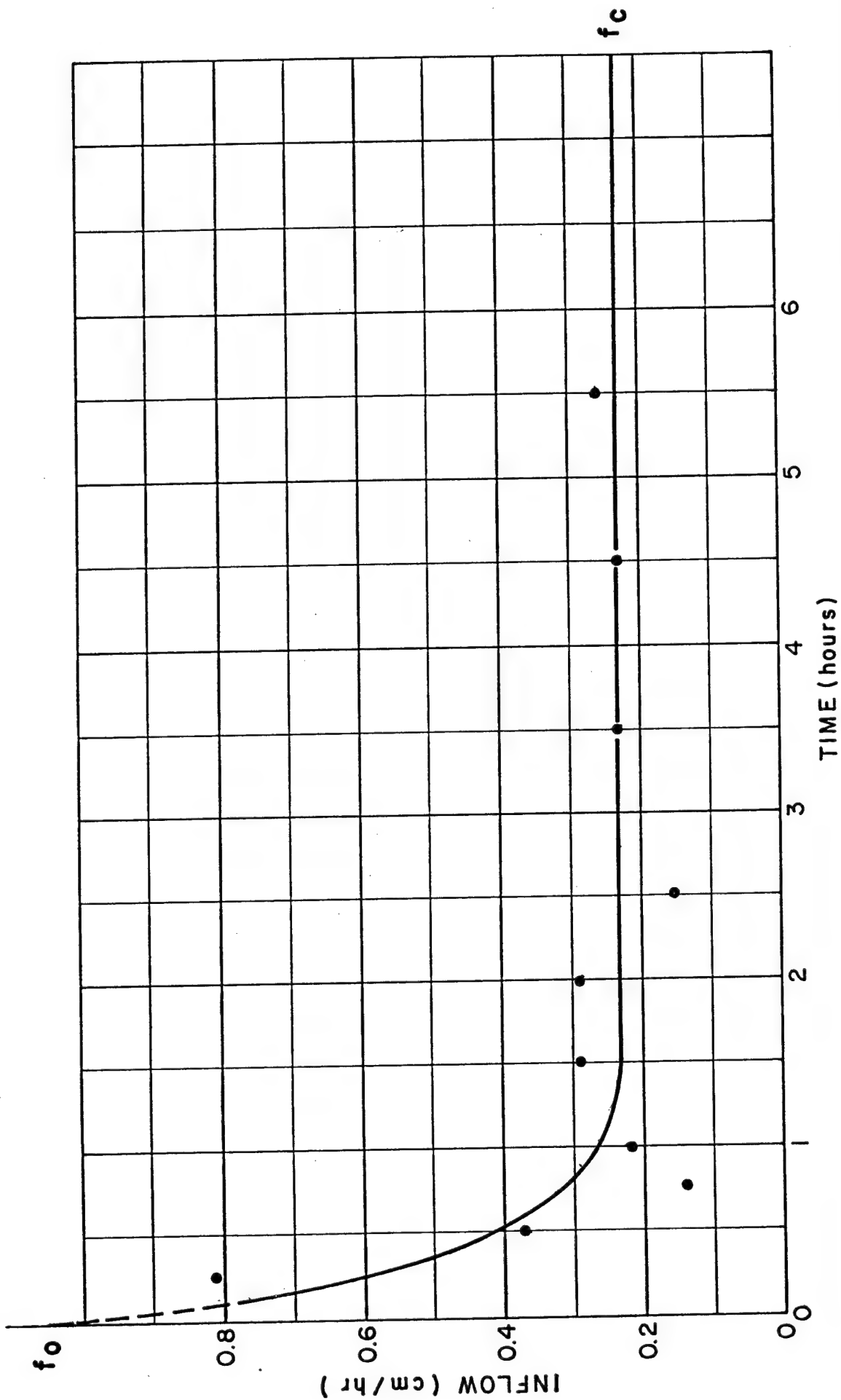


Fig. 10.

INFILTRATION SITE No.5

ROCKY MOUNTAIN ARSENAL
DENVER, COLORADO

RESOURCE CONSULTANTS, INC. - FORT COLLINS, COLORADO

7/14/83

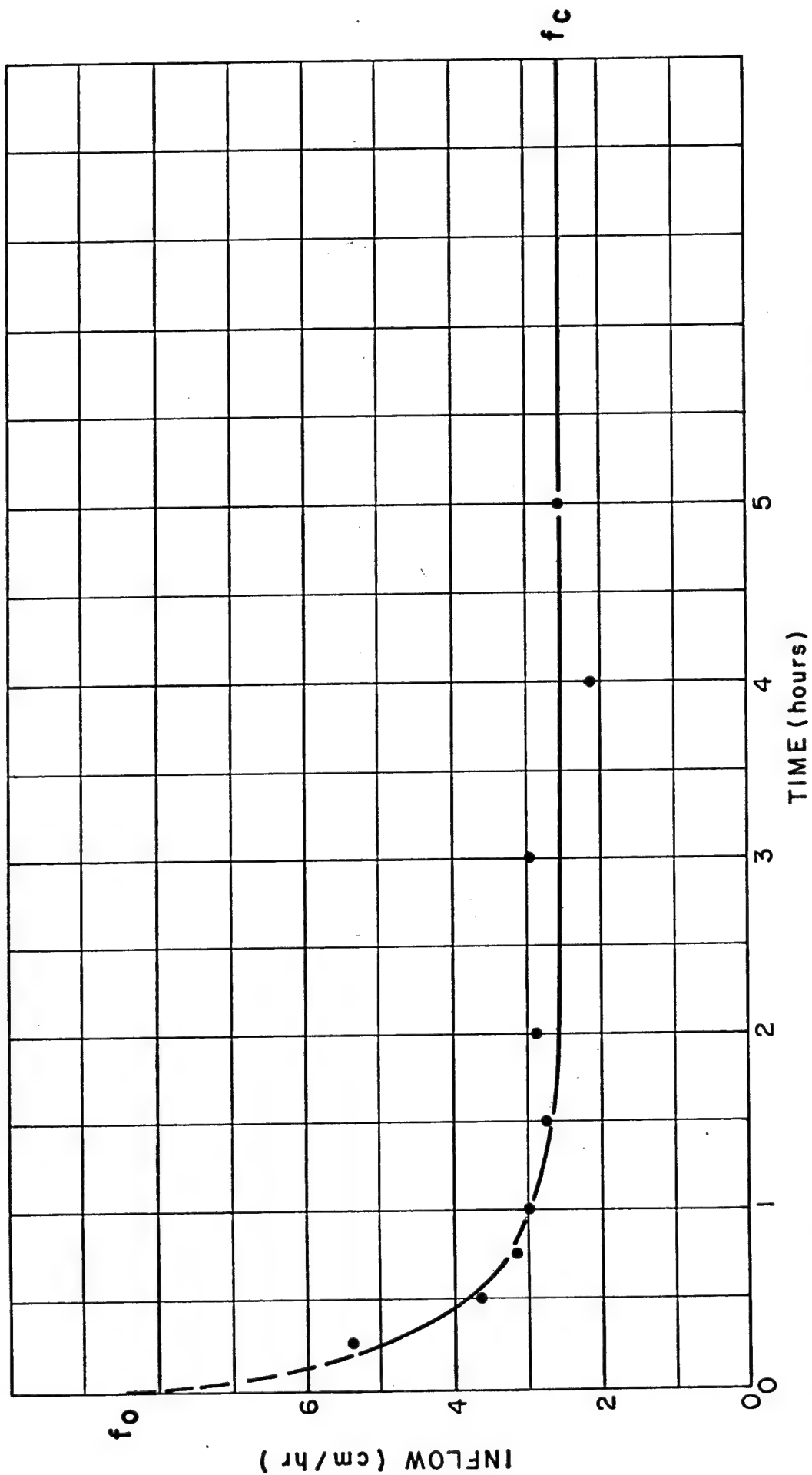


Fig. 11.

INFILTRATION SITE No. 6

7/14/83

**ROCKY MOUNTAIN ARSENAL
DENVER, COLORADO**

RESOURCE CONSULTANTS, INC. - FORT COLLINS, COLORADO

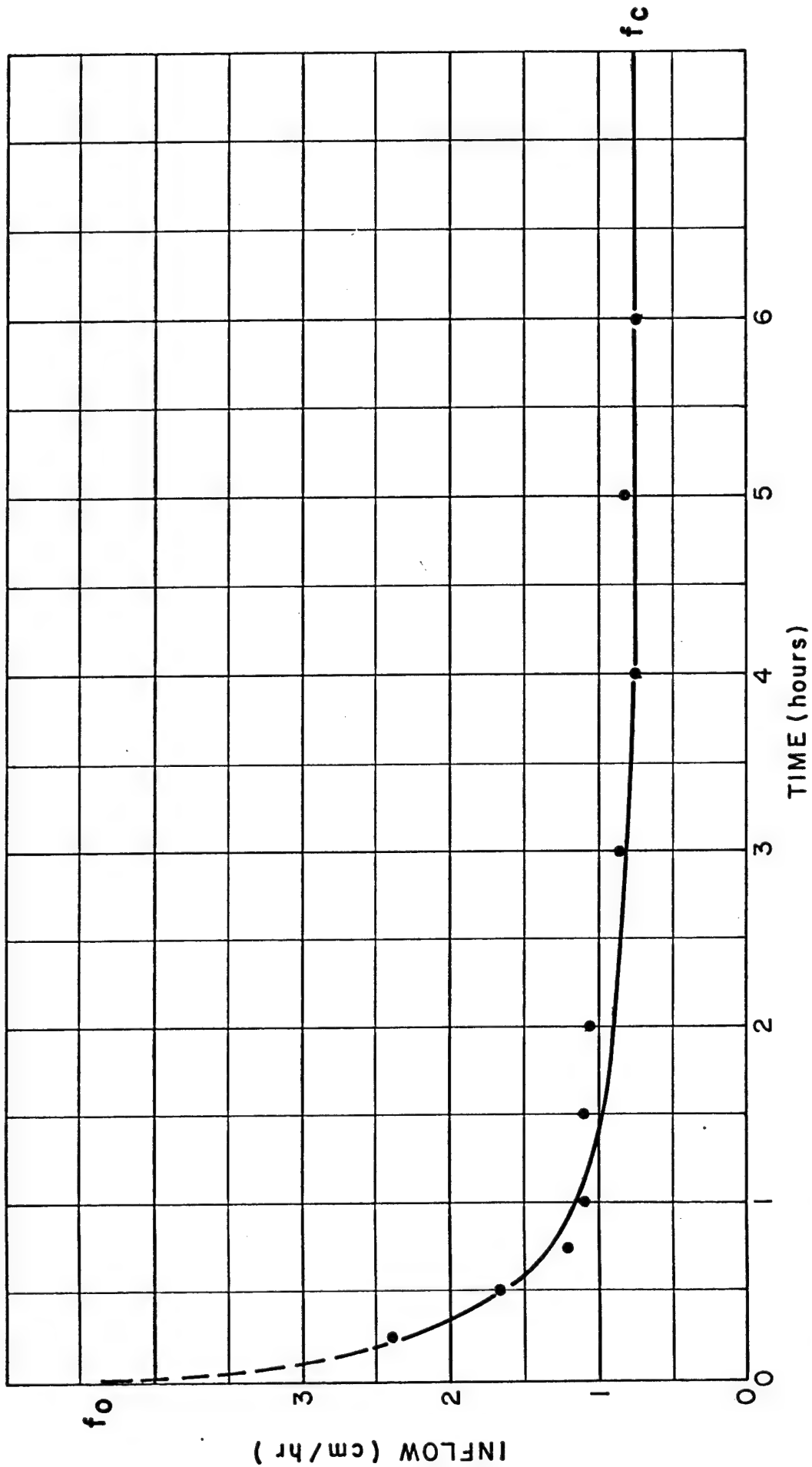


Fig. 12.

INFILTRATION SITE No. 7

7/13/83

ROCKY MOUNTAIN ARSENAL
DENVER, COLORADO

RESOURCE CONSULTANTS, INC. - FORT COLLINS, COLORADO

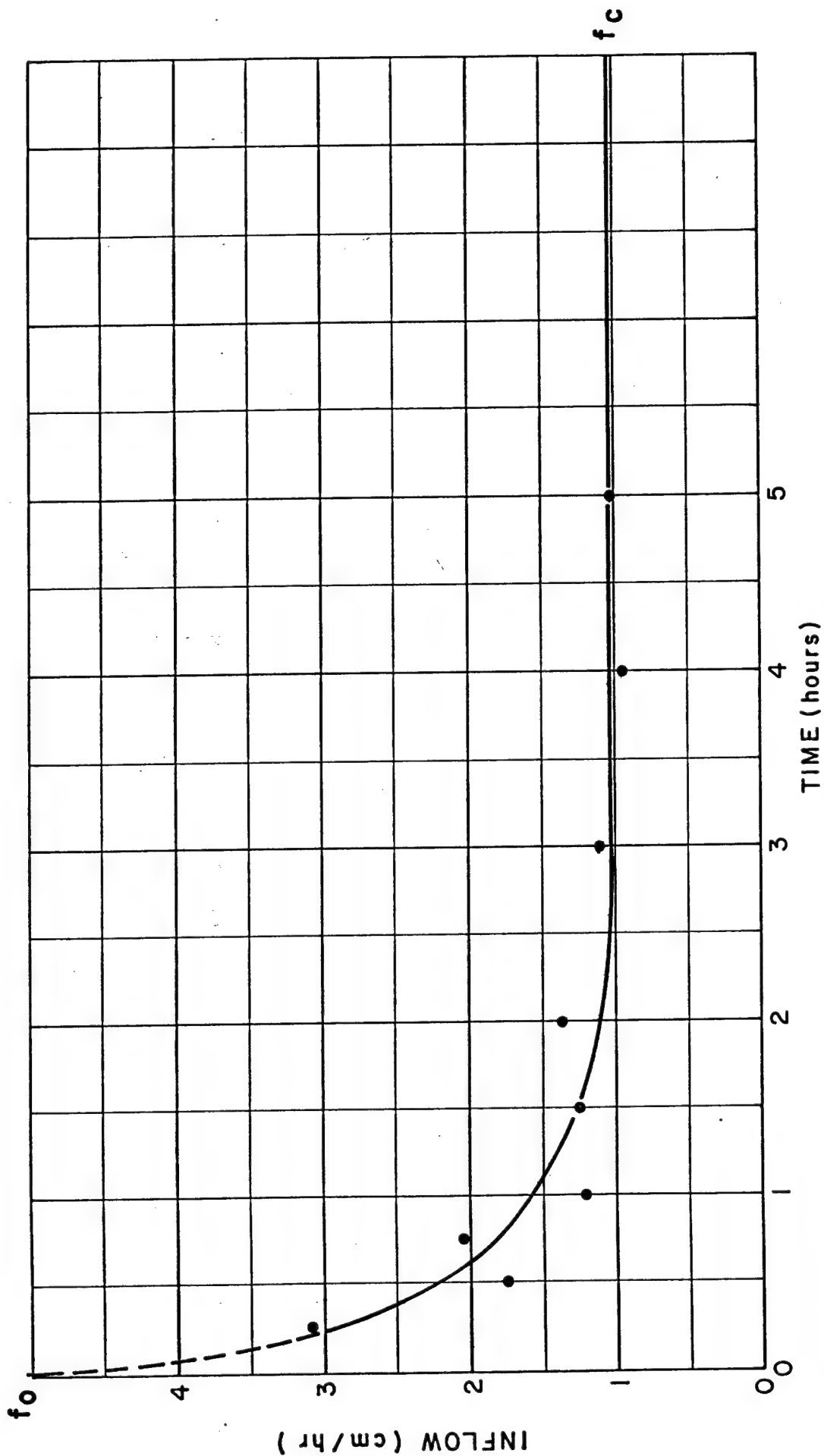


Fig. 13.

INFILTRATION SITE No. 8

7/13/83

ROCKY MOUNTAIN ARSENAL
DENVER, COLORADO

RESOURCE CONSULTANTS, INC. - FORT COLLINS, COLORADO

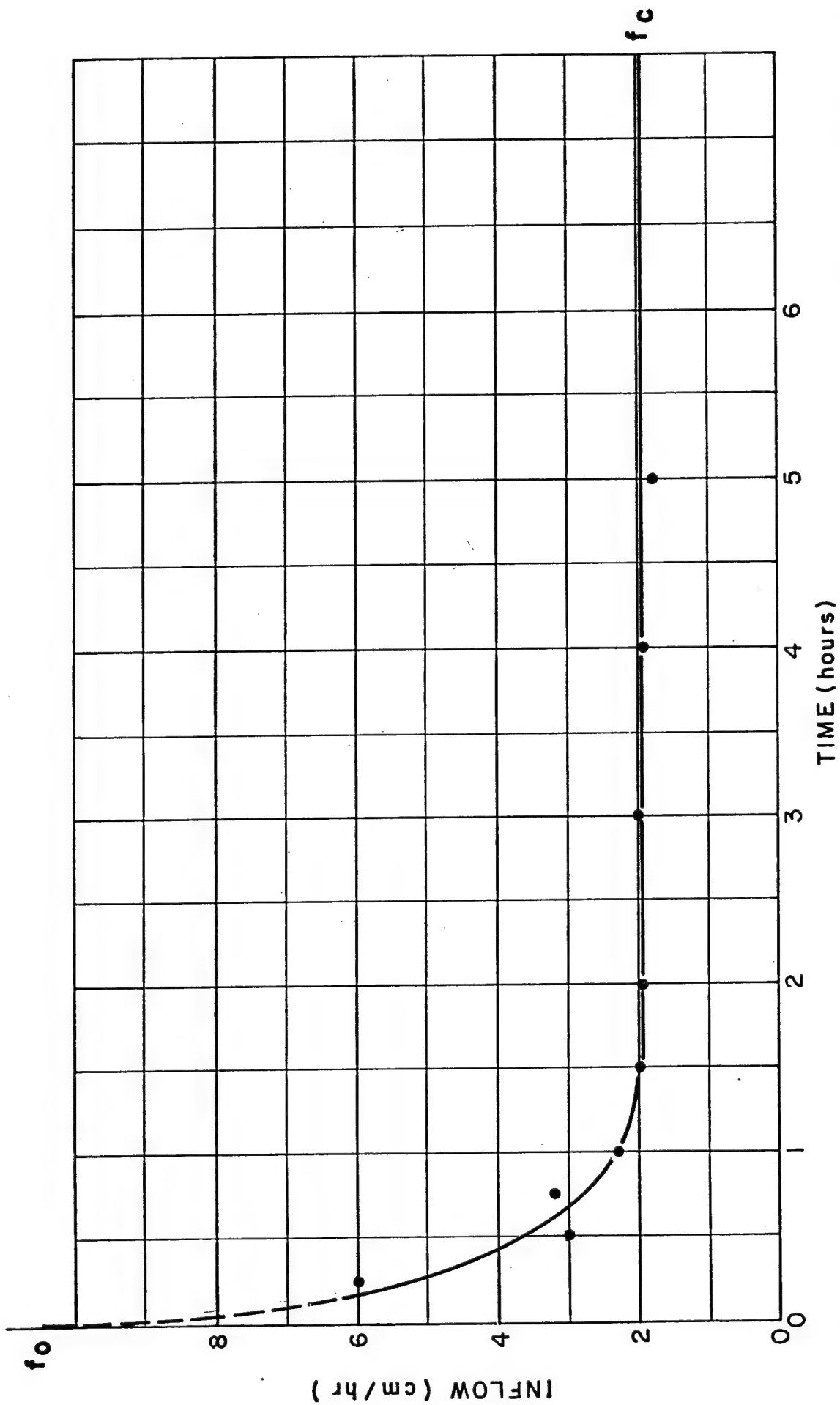


Fig. 14.

INFILTRATION SITE No.9

7/13/83

ROCKY MOUNTAIN ARSENAL
DENVER, COLORADO

RESOURCE CONSULTANTS, INC. - FORT COLLINS, COLORADO

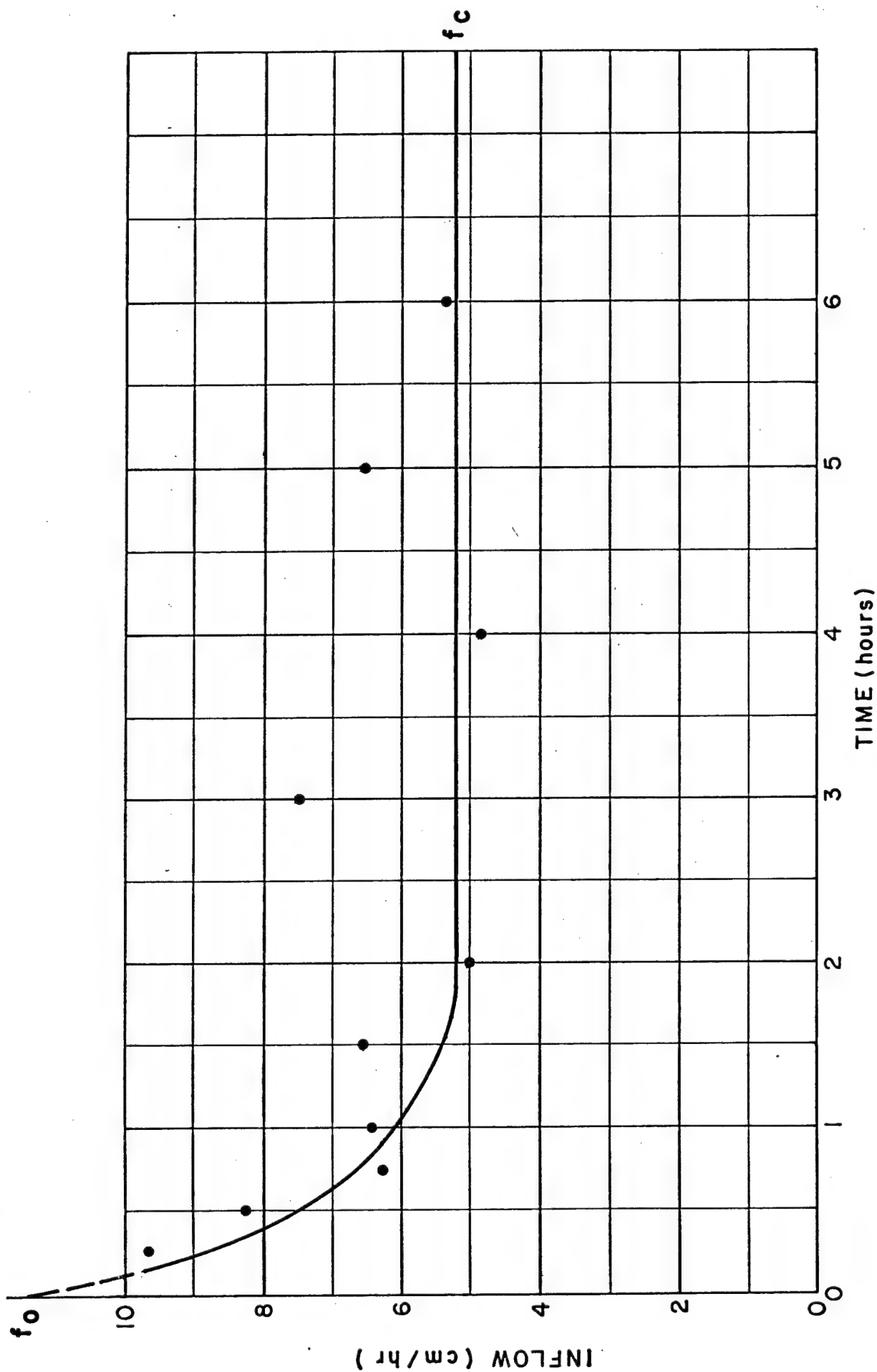


Fig. 15.

INFILTRATION SITE No.10

7/13/83

ROCKY MOUNTAIN ARSENAL
DENVER, COLORADO

RESOURCE CONSULTANTS, INC. - FORT COLLINS, COLORADO

Recommendations and Conclusions

Data in this report are based on one series of tests only. If this information is to be used for design purposes, the series should be repeated. Site #4 appears to be a difficult site for infiltration tests. It is recommended that this site be moved to a more favorable location.

Data in Table 1 indicate some very low values of infiltration rates. Any value less than about 0.1 centimeters per hour should be considered as impermeable for surface-water runoff computations.

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Johnson, A. I., 1963, A Field Method for Measurement of Infiltration, U. S. Geological Survey Water-Supply Paper 1544-F, U. S. Government Printing Office, Washington, DC, 27 pages.

USDA, Soil Conservation Service & Colo. Ag. Exper. Station, 1974, Soil Survey of Adams County, Colorado.

APPENDIX B

Numerical Data for Test Sites

ROCKY MOUNTAIN ARSENAL INFILTRATION TESTS
JULY 1983

| SITE # | DATE | TIME | AREA (CM**2) | INTERVAL (MIN) | (HOURS) | TOTAL HOURS | VOL (ML) | INFLOW (CM/HR) |
|--------|---------|------|-----------------|-------------------|---------|----------------|-------------|-------------------|
| 1 | 7/14/83 | 650 | 729.66 | 0 | 0 | 0 | 0 | 0 <u>1/</u> |
| | | 705 | 729.66 | 15 | .25 | .25 | 60 | .33 |
| | | 1105 | 729.66 | 240 | 4.00 | 4.25 | 110 | .04 |
| | | 1325 | 729.66 | 140 | 2.33 | 6.58 | 200 | .12 |
| | 7/15/83 | 615 | 729.66 | 1010 | 16.83 | 23.42 | 1320 | .11 |
| | | 1100 | 729.66 | 285 | 4.75 | 28.17 | 110 | .03 |
| 2 | 7/14/83 | 657 | 729.66 | 0 | 0 | 0 | 0 | 0 |
| | | 712 | 729.66 | 15 | .25 | .25 | 140 | .77 |
| | | 1112 | 729.66 | 240 | 4.00 | 4.25 | 120 | .04 |
| | | 1332 | 729.66 | 140 | 2.33 | 6.58 | 130 | .08 |
| | 7/15/83 | 630 | 729.66 | 1018 | 16.97 | 23.55 | 80 | .01 |
| | | 1105 | 729.66 | 275 | 4.58 | 28.13 | 1 | .00 |
| 3 | 7/14/15 | 922 | 729.66 | 0 | 0 | 0 | 0 | 0 |
| | | 1122 | 729.66 | 120 | 2.00 | 2.00 | 40 | .03 |
| | 7/15/83 | 640 | 729.66 | 1158 | 19.30 | 21.30 | 560 | .04 |
| | | 1110 | 729.66 | 270 | 4.50 | 25.80 | 110 | .03 |
| 4 | 7/14/83 | 916 | 729.66 | 0 | 0 | 0 | 0 | 0 |
| | | 931 | 729.66 | 15 | .25 | .25 | 3810 | 20.89 |
| | | 950 | 729.66 | 19 | .32 | .57 | 4670 | 20.21 |
| | | 1005 | 729.66 | 15 | .25 | .82 | 5900 | 32.34 |
| | | 1015 | 729.66 | 10 | .17 | .98 | 4500 | 37.00 |
| | | 1025 | 729.66 | 10 | .17 | 1.15 | 2610 | 21.46 |
| | | 1035 | 729.66 | 10 | .17 | 1.32 | 2590 | 21.30 |
| | | 1045 | 729.66 | 10 | .17 | 1.48 | 2260 | 18.58 |
| | | 1055 | 729.66 | 10 | .17 | 1.65 | 2440 | 20.06 |
| | | 1125 | 729.66 | 30 | .50 | 2.15 | 7410 | 20.31 |
| | | 1155 | 729.66 | 30 | .50 | 2.65 | 7750 | 21.24 |
| | | 1235 | 729.66 | 40 | .67 | 3.32 | 8180 | 16.82 |
| | | 1315 | 729.66 | 40 | .67 | 3.98 | 6730 | 13.84 |
| | | 1345 | 729.66 | 30 | .50 | 4.48 | 4260 | 11.68 |
| 5 | 7/14/83 | 837 | 729.66 | 0 | 0 | 0 | 0 | 0 |
| | | 852 | 729.66 | 15 | .25 | .25 | 147 | .81 |
| | | 907 | 729.66 | 15 | .25 | .50 | 68 | .37 |
| | | 922 | 729.66 | 15 | .25 | .75 | 25 | .14 |
| | | 937 | 729.66 | 15 | .25 | 1.00 | 40 | .22 |
| | | 1007 | 729.66 | 30 | .50 | 1.50 | 105 | .29 |
| | | 1037 | 729.66 | 30 | .50 | 2.00 | 105 | .29 |
| | | 1107 | 729.66 | 30 | .50 | 2.50 | 55 | .15 |
| | | 1207 | 729.66 | 60 | 1.00 | 3.50 | 170 | .23 |
| | | 1307 | 729.66 | 60 | 1.00 | 4.50 | 170 | .23 |
| | | 1407 | 729.66 | 60 | 1.00 | 5.50 | 190 | .26 |

1/ Zero indicates "no data."

ROCKY MOUNTAIN ARSENAL INFILTRATION TESTS JULY 1983

| SITE # | DATE | TIME | AREA (CM**2) | INTERVAL (MIN) (HOURS) | | TOTAL HOURS | VOL (ML) | INFLOW (CM/HR) |
|--------|---------|------|-----------------|---------------------------|------|----------------|-------------|-------------------|
| 6 | 7/14/83 | 900 | 729.66 | 0 | 0 | 0 | 0 | 0 <u>1</u> / |
| | | 915 | 729.66 | 15 | .25 | .25 | 975 | 5.34 |
| | | 930 | 729.66 | 15 | .25 | .50 | 665 | 3.65 |
| | | 945 | 729.66 | 15 | .25 | .75 | 575 | 3.15 |
| | | 1000 | 729.66 | 15 | .25 | 1.00 | 545 | 2.99 |
| | | 1030 | 729.66 | 30 | .50 | 1.50 | 1000 | 2.74 |
| | | 1100 | 729.66 | 30 | .50 | 2.00 | 1055 | 2.89 |
| | | 1200 | 729.66 | 60 | 1.00 | 3.00 | 2170 | 2.97 |
| | | 1300 | 729.66 | 60 | 1.00 | 4.00 | 1545 | 2.12 |
| | | 1400 | 729.66 | 60 | 1.00 | 5.00 | 1870 | 2.56 |
| 7 | 7/13/83 | 1211 | 729.66 | 0 | 0 | 0 | 0 | 0 |
| | | 1226 | 729.66 | 15 | .25 | .25 | 438 | 2.40 |
| | | 1241 | 729.66 | 15 | .25 | .50 | 304 | 1.67 |
| | | 1256 | 729.66 | 15 | .25 | .75 | 219 | 1.20 |
| | | 1311 | 729.66 | 15 | .25 | 1.00 | 201 | 1.10 |
| | | 1341 | 729.66 | 30 | .50 | 1.50 | 393 | 1.08 |
| | | 1411 | 729.66 | 30 | .50 | 2.00 | 384 | 1.05 |
| | | 1511 | 729.66 | 60 | 1.00 | 3.00 | 624 | .86 |
| | | 1611 | 729.66 | 60 | 1.00 | 4.00 | 560 | .77 |
| | | 1711 | 729.66 | 60 | 1.00 | 5.00 | 600 | .82 |
| | | 1811 | 729.66 | 60 | 1.00 | 6.00 | 540 | .74 |
| 8 | 7/13/83 | 1350 | 729.66 | 0 | 0 | 0 | 0 | 0 |
| | | 1405 | 729.66 | 15 | .25 | .25 | 560 | 3.07 |
| | | 1420 | 729.66 | 15 | .25 | .50 | 320 | 1.75 |
| | | 1435 | 729.66 | 15 | .25 | .75 | 370 | 2.03 |
| | | 1450 | 729.66 | 15 | .25 | 1.00 | 220 | 1.21 |
| | | 1520 | 729.66 | 30 | .50 | 1.50 | 460 | 1.26 |
| | | 1550 | 729.66 | 30 | .50 | 2.00 | 500 | 1.37 |
| | | 1650 | 729.66 | 60 | 1.00 | 3.00 | 820 | 1.12 |
| | | 1750 | 729.66 | 60 | 1.00 | 4.00 | 700 | .96 |
| | | 1850 | 729.66 | 60 | 1.00 | 5.00 | 750 | 1.03 |
| 9 | 7/13/83 | 1324 | 729.66 | 0 | 0 | 0 | 0 | 0 |
| | | 1339 | 729.66 | 15 | .25 | .25 | 1092 | 5.99 |
| | | 1354 | 729.66 | 15 | .25 | .50 | 459 | 2.52 |
| | | 1409 | 729.66 | 15 | .25 | .75 | 589 | 3.23 |
| | | 1424 | 729.66 | 15 | .25 | 1.00 | 424 | 2.32 |
| | | 1454 | 729.66 | 30 | .50 | 1.50 | 716 | 1.96 |
| | | 1524 | 729.66 | 30 | .50 | 2.00 | 713 | 1.95 |
| | | 1624 | 729.66 | 60 | 1.00 | 3.00 | 1452 | 1.99 |
| | | 1724 | 729.66 | 60 | 1.00 | 4.00 | 1410 | 1.93 |
| | | 1824 | 729.66 | 60 | 1.00 | 5.00 | 1310 | 1.80 |
| 10 | 7/13/83 | 1230 | 729.66 | 0 | 0 | 0 | 0 | 0 |
| | | 1245 | 729.66 | 15 | .25 | .25 | 1760 | 9.65 |
| | | 1300 | 729.66 | 15 | .25 | .50 | 1510 | 8.28 |
| | | 1315 | 729.66 | 15 | .25 | .75 | 1140 | 6.25 |
| | | 1330 | 729.66 | 15 | .25 | 1.00 | 1170 | 6.41 |
| | | 1400 | 729.66 | 30 | .50 | 1.50 | 2390 | 6.55 |
| | | 1430 | 729.66 | 30 | .50 | 2.00 | 1820 | 4.99 |
| | | 1530 | 729.66 | 60 | 1.00 | 3.00 | 5460 | 7.48 |
| | | 1645 | 729.66 | 75 | 1.25 | 4.25 | 4420 | 4.85 |
| | | 1730 | 729.66 | 45 | .75 | 5.00 | 3560 | 6.51 |
| | | 1830 | 729.66 | 60 | 1.00 | 6.00 | 3900 | 5.34 |

1/ Zero indicates "no data."